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# Ink-Jet Printed Graphene Electronics

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## Abstract

We demonstrate ink-jet printing as a viable method for large area fabrication of graphene devices. We produce a graphene-based ink by liquid phase exfoliation of graphite in N-Methylpyrrolidone. We use it to print thin-film transistors, with mobilities up to  $\sim 95 \text{cm}^2 \text{V}^{-1} \text{s}^{-1}$ , as well as transparent and conductive patterns, with  $\sim 80\%$  transmittance and  $\sim 30 \text{k}\Omega/\square$  sheet resistance. This paves the way to all-printed, flexible and transparent graphene devices on arbitrary substrates.

## Introduction

Flexible electronics is a rapidly expanding research area.<sup>1</sup> Applications include touch screens,<sup>2</sup> electronic paper (e-paper),<sup>3,4</sup> sensors,<sup>5</sup> radio frequency tags,<sup>6</sup> photovoltaic cells,<sup>7,8</sup> and electronic textiles.<sup>9</sup> To date, it mainly relies on two fabrication strategies: one in which substrates bearing thousands of Field-effect Transistors (FETs) are bonded to plastic by transfer printing or pick-and place methods;<sup>10</sup> another in which FETs are prepared directly on the target substrate by several coating, curing and lithographic steps.<sup>1,11</sup> Rubber stamping,<sup>12</sup> embossing<sup>13</sup> and ink-jet printing<sup>14,15</sup> reduce the number of such fabrication steps.

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4 Ink-jet printing is one of the most promising techniques for large area fabrication of flexible  
5 plastic electronics.<sup>15</sup> A range of components can be printed, such as transistors,<sup>13,15–18</sup> photo-  
6 voltaic devices,<sup>19</sup> organic light emitting diodes (OLEDs),<sup>13,18,20</sup> and displays.<sup>13</sup> Ink-jet printing  
7 is versatile,<sup>18</sup> involves a limited number of process steps,<sup>21</sup> is amenable for mass production, and  
8 can deposit controlled amounts of material.<sup>21</sup> Drop on demand<sup>21,22</sup> ink-jet printing has progressed  
9 from printing text and graphics,<sup>21</sup> to a tool for rapid manufacturing,<sup>23</sup> being now a well established  
10 technique to print Thin Film Transistor (TFT) based on organic conducting and semiconducting  
11 inks.<sup>5,15,24</sup> However, their mobilities,  $\mu < 0.5 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ ,<sup>5,18</sup> are still much lower than standard  
12 silicon technology. Several approaches aim to improve these results, such as the use of polysil-  
13 icon,<sup>25</sup> zinc oxide nanoparticles<sup>26</sup> and carbon nanotubes (CNTs).<sup>27–32</sup> Metal nanoparticle inks  
14 are not stable in ordinary solvents, such as Deionized (DI) Water, Acetone, Isopropyl Alcohol,  
15 N-Methylpyrrolidone (NMP), Tetrahydrofuran.<sup>18,33</sup> Therefore they need to be chemically modi-  
16 fied in order to be dispersed,<sup>18</sup> via the use of stabilizers, which usually degrade in a couple of  
17 years.<sup>18,33</sup> Metal nanoparticles also tend to oxidize after the printing process.<sup>18,33</sup> Ink-jet printed  
18 CNT-TFTs have been reported with  $\mu$  up to  $50 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$  and a ON/OFF ratio  $\sim 10^3$ .<sup>32</sup>

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34 Graphene is the two-dimensional (2d) building block for  $sp^2$  carbon allotropes of every other  
35 dimensionality. It can be stacked into 3d graphite, rolled into 1d nanotubes, or wrapped into 0d  
36 fullerenes.<sup>34</sup> It is at the centre of an ever expanding research area.<sup>34–37</sup> Near-ballistic transport and  
37 high mobility make it an ideal material for nanoelectronics, especially for high frequency applica-  
38 tions.<sup>38</sup> Furthermore, its optical and mechanical properties are ideal for micro and nanomechanical  
39 systems, thin-film transistors, transparent and conductive composites and electrodes, and photon-  
40 ics.<sup>34,37,39</sup> Graphene was isolated by micromechanical exfoliation of graphite.<sup>40</sup> This technique  
41 still gives the best samples in terms of purity, defects, mobility and optoelectronics properties.  
42 However, large scale production approaches are needed for widespread application. These encom-  
43 pass growth by chemical vapor deposition (CVD),<sup>41–46</sup> segregation by heat treatment of silicon  
44 carbide<sup>47–50</sup> and metal substrates,<sup>51–54</sup> liquid phase exfoliation (LPE).<sup>55–58</sup> Amongst these, LPE  
45 is ideally suited to produce printable inks.  
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4 Graphite can be exfoliated by chemical wet dispersion followed by ultrasonication, both in  
5 aqueous<sup>56,58</sup> and non-aqueous solvents.<sup>55,58</sup> Dispersions can be achieved by mild sonication of  
6 graphite in water with Sodium Deoxycholate followed by sedimentation based-ultracentrifugation.<sup>58,59</sup>  
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8 Bile salt surfactants also allow the isolation of flakes with controlled thickness, when combined  
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10 with density gradient ultracentrifugation (DGU).<sup>60</sup> Exfoliation of graphite intercalated compounds<sup>57</sup>  
11 and expandable graphite<sup>61</sup> was also reported.  
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15 LPE was first achieved through sonication of graphite oxide,<sup>62</sup> following the Hummers method.<sup>63</sup>  
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17 The oxidation of graphite in the presence of acids and oxidants<sup>64,65</sup> disrupts the sp<sup>2</sup>-network and  
18 introduces hydroxyl or epoxide groups,<sup>66,67</sup> with carboxylic or carbonyl groups attached to the  
19 edge.<sup>66,67</sup> These make GO sheets readily dispersible in water<sup>62,68</sup> and several other solvents.<sup>69</sup>  
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21 Although large GO flakes can be produced, these are intrinsically defective,<sup>62,70</sup> and electrically  
22 insulating.<sup>62,66</sup> Despite several attempts,<sup>62,66</sup> reduced GO (RGO) does not fully regain the pris-  
23 tine graphene electrical conductivity.<sup>66,71</sup> It is thus important to distinguish between dispersion  
24 processed graphene flakes,<sup>55-58</sup> retaining the electronic properties of graphene, and insulating GO  
25 dispersions.<sup>62,71</sup> Several groups reported GO-based inks.<sup>33,72,73</sup> Ref.<sup>72</sup> ink-jet printed RGO films  
26 for sensors applications, while Ref.<sup>33</sup> produced RGO-stabilized Cu nanoparticles as low temper-  
27 ature metal colloids, to replace standard metal nanoparticle inks, that require high temperature  
28 sintering postprocessing.<sup>74</sup> Mobilities up to  $90\text{cm}^2\text{V}^{-1}\text{s}^{-1}$  have been achieved for highly reduced  
29 GO films by ink-jet printing,<sup>73</sup> with an ON/OFF ratio up to 10.<sup>73</sup>  
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42 Here we produce a graphene-based ink and demonstrate its viability for printed electronics.  
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## 46 **Results and discussion**

### 47 **Ink requirements**

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51 A key property of inks viable for printing is their ability to generate droplets.<sup>75,76</sup> Ink viscos-  
52 ity,  $\eta$  [mPa s], surface tension,  $\gamma$  [mJ m<sup>-2</sup>], density,  $\rho$  [g cm<sup>-3</sup>], and nozzle diameter,  $a$  [ $\mu\text{m}$ ],  
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influence the spreading of the resulting liquid drops.<sup>75-77</sup> These can be arranged into dimensionless figures of merit (FOM), such as the Reynolds (Re),<sup>75-77</sup> Weber (We),<sup>75-77</sup> and Ohnesorge (Oh)<sup>75-77</sup> numbers:  $Re = \frac{v\rho a}{\eta}$ ;  $We = \frac{v^2\rho a}{\gamma}$ ,  $Oh = \frac{\sqrt{We}}{Re} = \frac{\eta}{\sqrt{\gamma\rho a}}$ , where  $v$ [m/s] is the drop velocity.

Refs.<sup>75-77</sup> suggested to use  $Z=1/Oh$  as the appropriate FOM to characterize drop formation,  $1 < Z < 14$  being required to get stable drop generation.<sup>75,76</sup> For  $Z < 1$  the high viscosity prevents drop ejection,<sup>75,76</sup> whereas at  $Z > 14$  the primary drop is accompanied by a number of satellite droplets.<sup>75,76</sup> Moreover, when inks contain dispersed molecules or nano-particles, the latter should be smaller than the nozzle diameter, to prevent clogging.<sup>21,23</sup> Refs.<sup>23,78</sup> suggested that the size of such molecules or particles should be at least 1/50 of the nozzle diameter, in order to exclude any printing instability, such as clustering of the particles at the nozzle edge, which may deviate the drop trajectory, or result in agglomerates that will eventually block the nozzle.

The ejected drop behavior on the substrate can be efficiently described by fluid dynamics. When a small liquid droplet is in contact with a flat surface, partial wetting results in a finite angle between the liquid and the substrate,<sup>79</sup> known as contact angle,  $\theta_C$ .<sup>79-81</sup> The lower drop size limit is given by<sup>75,76</sup>  $s[\mu m] = a \sqrt{\frac{We+12}{3(1-\cos\theta_C)+4We/Re^{1/2}}}$ . Thus, e.g., for a typical  $a=50\mu m$ ,  $We=20$ ,  $Re=58$  and  $\theta_C \sim 45^\circ$ , we get  $s \sim 85-90\mu m$ . The distance from the substrate must be optimized to guarantee both homogeneous printing and the highest resolution, barring any unusual jetting conditions, such as perturbations from the surrounding environment and diversion of the drop trajectory.<sup>18,75,82</sup> Furthermore, a substrate very close to the nozzle causes secondary drops to scatter off during the impact of the primary drop,<sup>18,83</sup> due to the initial drop jetting pressure, thus affecting the homogeneity of the final printed features.<sup>83</sup> The final assembly of printed nano-particle inks depends on the substrate Surface Energy (SE),<sup>21,23</sup> as well as the ink viscosity and surface tension.<sup>21</sup>

When a drop of an ink containing dispersed particles evaporates on a surface it commonly leaves a dense, ring-like, deposit along its perimeter.<sup>21,23</sup> This is the so-called "coffee ring effect",<sup>84</sup> i.e. a distortion of the drops during solvent drying due to the interplay of ink viscosity and solute transport via solvent motion (arising from surface tension interaction between solvent and substrate).<sup>18,84</sup> This is one of the most important phenomena affecting the homogeneity of

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3 ink-jet printed drops.<sup>18,84</sup> In order to prevent this, it is necessary to "freeze" the drops geometry  
4 immediately after they form an homogeneous and continuous film on the substrate.<sup>18</sup>  
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7 Here we use an ink-jet printer with a nozzle diameter  $\sim 50\mu\text{m}$ , thus we need to have flakes less  
8 than  $1\mu\text{m}$  across. By tuning  $\eta$ ,  $\gamma$  and  $\rho$  we will target a Z within the optimal range. We print on  
9 Si/SiO<sub>2</sub> (because we want to probe the electrical properties of our graphene-ink) and borosilicate  
10 (Pyrex 7740-Polished Prime Grade) glass substrates (because we want to test graphene-ink as  
11 transparent conductor), both with a roughness  $R_z < 15\text{nm}$ . Our aim is to obtain ink-jet printed drops,  
12 on substrate, with homogeneous flakes and uniform morphology, i.e. with roughness comparable to  
13 the substrate. We obtain this by varying the contact angle and optimizing the substrate wettability.  
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22 In order to reduce the coffee ring effect we need both a solvent with boiling point ( $T_c$  [ $^{\circ}\text{C}$ ])  
23 and heat of vaporization ( $V_c$  [kJ/mol]) higher than water,<sup>18,82,84</sup> and a substrate which promotes  
24 adhesion.<sup>85</sup> Thus we use NMP as solvent for two main reasons. First, it has higher boiling point  
25 ( $\sim 202^{\circ}\text{C}$ )<sup>86</sup> and heat of vaporization (54.5kJ/mol),<sup>86</sup> than water ( $\sim 100^{\circ}\text{C}$  and  $\sim 40\text{kJ/mol}$ ). Sec-  
26 ond, NMP is the best solvent to get high-yield, surfactant-free exfoliation of graphite.<sup>55,58</sup> We then  
27 test several surface treatments to optimize substrate adhesion. After printing NMP is removed by  
28 a thermal annealing at  $170^{\circ}\text{C}$  for 5 minutes.  
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## 38 **Graphene-based printable ink**

39 We prepare the graphene-based printable ink as follows. Graphite flakes (NGS Naturgraphit)  
40 are sonicated (Decon bath, 20W) in NMP for 9 hours. The un-exfoliated flakes are left to settle  
41 for 10 mins after sonication. The decanted dispersions are then ultracentrifuged using a TH-641  
42 swinging bucket rotor in a Sorvall WX-100 Ultra-centrifuge at 10,000 rpm ( $\sim 15,000g$ ) for an hour  
43 and filtered to remove flakes  $> 1\mu\text{m}$ , that might clog the nozzle. The resulting ink is characterized  
44 by Optical Absorption Spectroscopy (OAS), High Resolution Transmission Electron Microscopy  
45 (HRTEM), Electron diffraction and Raman spectroscopy (see Methods).  
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55 OAS can be used to estimate the concentration of graphene<sup>55,56,59</sup> using the Beer-Lambert Law  
56 according to the relation  $A = \alpha cl$ , where  $A$  is the absorbance,  $l$  [m] is the light path length,  $c$  [g/L]  
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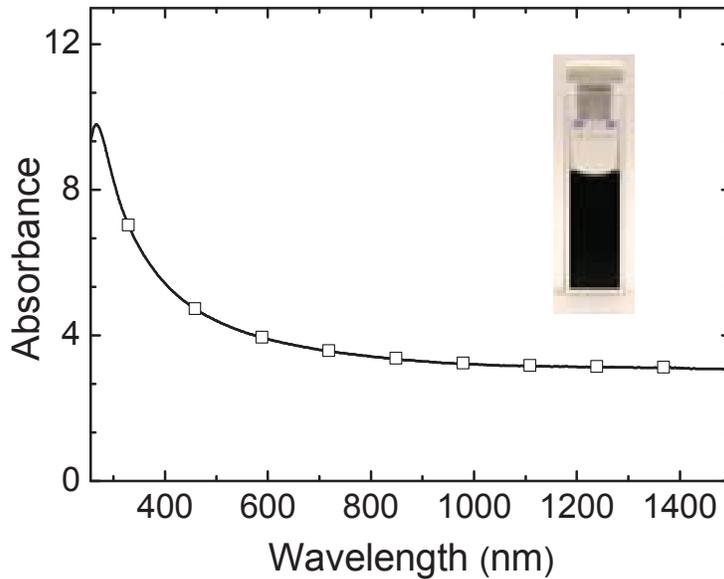


Figure 1: Absorbance of our graphene-ink. The inset is a picture of a vial of ink.

the concentration of dispersed graphitic material and  $\alpha$  [ $\text{L g}^{-1} \text{m}^{-1}$ ] the absorption coefficient. Figure 1 plots an OAS spectrum of our ink diluted to 10%. The ink is diluted to avoid strong scattering losses at higher concentrations, which could cause deviation of the measured value of  $A$  from the Beer-Lambert law. The spectrum in Figure 1 is mostly featureless, as expected due to linear dispersion of the Dirac electrons,<sup>37,39,87–90</sup> the peak in the UV region being a signature of the van Hove singularity in the graphene density of states.<sup>88</sup> From  $\alpha \sim 1390 \text{Lg}^{-1} \text{m}^{-1}$  at 660nm, as for Refs.,<sup>56,58</sup> we estimate  $c \sim 0.11 \pm 0.02 \text{g/L}$ .

Figure 2a is HRTEM image of a Single Layer Graphene (SLG) flake from the ink, while Figure 2b is a normal-incidence electron diffraction of the same flake of Figure 2a. It shows the expected sixfold symmetry.<sup>91–93</sup> The peaks are labeled with the corresponding Miller-Bravais (hkil) indexes. For Few Layer Graphene (FLG) flakes with Bernal (AB) stacking, the intensity ratio  $I_{1100}/I_{2110}$  is  $<1$ , while for SLG  $I_{1010}/I_{2110} >1$ .<sup>91,93</sup> We use this to distinguish SLG from FLGs.<sup>55,59</sup> Figure 2c plots the diffraction intensity measured along the line section through the  $(1\bar{2}10)$ ,  $(0\bar{1}10)$ ,  $(\bar{1}010)$ ,  $(\bar{2}110)$  axis, reported in Figure 2b. The inner peaks,  $(0\bar{1}10)$  and  $(\bar{1}010)$ , are  $\sim 1.5$  times more intense than the outer ones,  $(1\bar{2}10)$  and  $(\bar{2}110)$ , indicating that the flake is SLG.<sup>91</sup> The analysis of the edges also gives a reliable information on the number of layers and can be used to investigate a

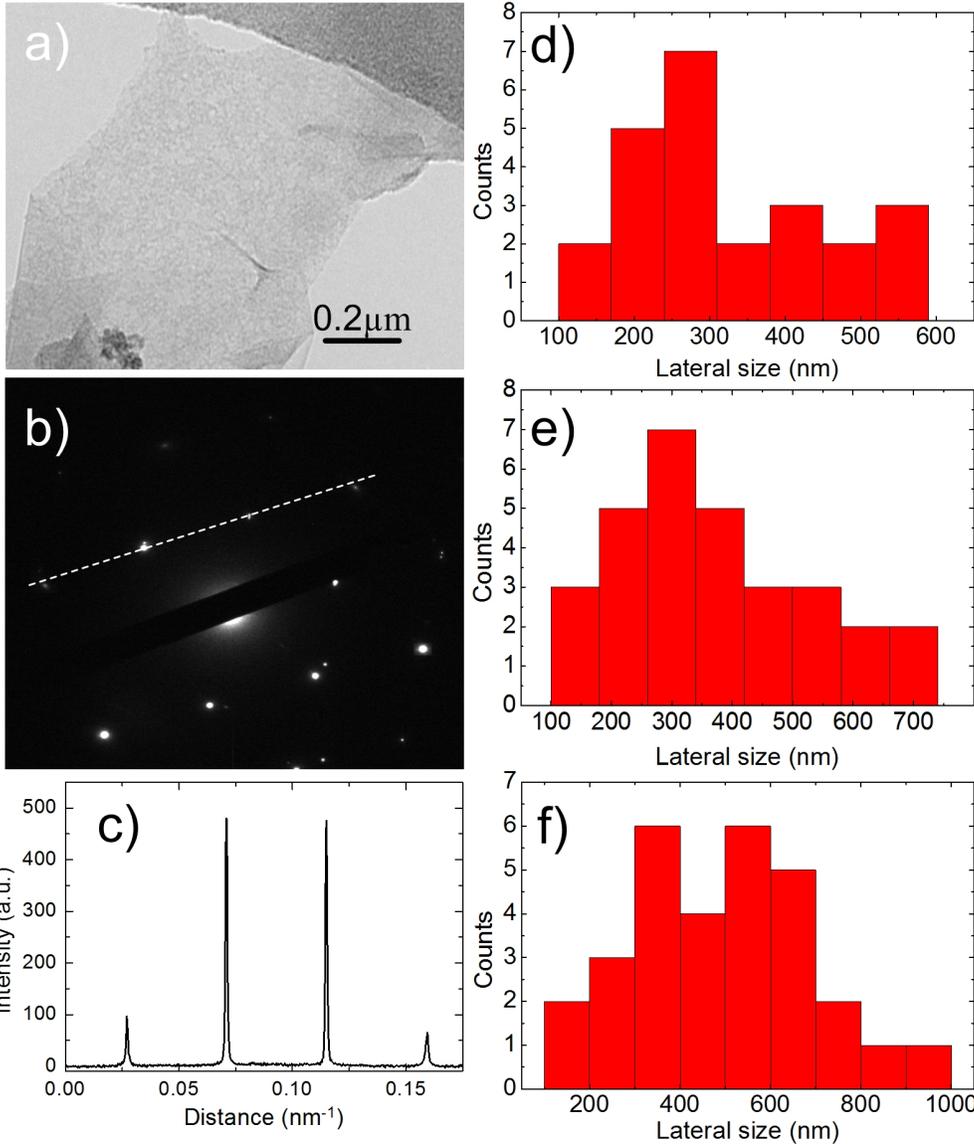


Figure 2: a,b) HRTEM image and electron diffraction pattern of dispersion-cast SLG. c) Diffracted intensity along the dashed line in b. Statistics of lateral size for d) SLGs, e) BLGs and f) FLGs.

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3 large number of flakes,<sup>91</sup> from zoomed-in high resolution edge images.<sup>55,94</sup> If SLG folds or several  
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5 SLGs stack one on the other, selected area diffraction is used to distinguish contentious cases.  
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8 These combined analysis show that our ink mostly consists of SLGs, Bi-Layers (BLG) and  
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10 FLGs, with lateral size  $\sim 300$ - $1000$ nm. We find that  $\sim 35\%$  SLGs are larger than  $300$ nm (Fig-  
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12 ure 2d);  $\sim 40\%$  BLGs are larger than  $350$ nm (Figure 2e);  $\sim 55\%$  FLGs are larger than  $450$ nm  
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14 (Figure 2f). In particular, we have  $33\%$  SLG with  $c \sim 0.11$ g/L. Previous works on LPE of graphene  
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16 in NMP reported up to  $\sim 28\%$  SLG for  $c \sim 0.18$ g/L<sup>58</sup> and  $\sim 21\%$  for  $c \sim 1.8$ g/L.<sup>94</sup> Ref.<sup>57</sup> also re-  
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18 ported exfoliation of intercalated graphite in NMP yielding  $\sim 20\%$  SLGs for  $c \sim 0.01$ g/L. Thus our  
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20 ink has higher SLG yield with respect to previous works, but lower  $c$  than ref.<sup>94</sup> This higher  $c$  was  
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22 achieved by long time (up to  $460$ h) ultrasonication.<sup>94</sup> However Ref.<sup>94</sup> reported defect formation  
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24 and reduction of size as a result. Our combination of low-power sonication ( $<25$ W) followed by  
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26 ultracentrifugation is ideal to obtain high yield of defect-free SLGs.  
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29 Stable dispersions require the Gibbs free energy of mixing,  $\Delta G_{mix}$ , to be zero or negative,<sup>95</sup>  
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31 where  $\Delta G_{mix} = \Delta H_{mix} - K\Delta S_{mix}$ ,  $K$  being the temperature,  $\Delta H_{mix}$  the enthalpy of mixing and  
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33 and  $\Delta S_{mix}$  the entropy change in the mixing process.<sup>55,95</sup> For graphene and nanotubes,  $\Delta S_{mix}$  is  
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35 small.<sup>55,96</sup> Therefore, for dispersion and stabilization of graphene in solvents,  $\Delta H_{mix}$  needs to be  
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37 very small. This can be achieved by choosing a solvent whose surface energy is very close to  
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39 that of graphene.<sup>55</sup> The surface energy of NMP satisfies this requirement and allows efficient ex-  
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41 foliation of graphite. Graphite can also be efficiently exfoliated in water with the use of bile salt  
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43 surfactants. Ref.<sup>97</sup> reported  $\sim 20\%$  SLGs and  $c \sim 0.3$ g/L SLGs, while Ref.<sup>59</sup> reported  $\sim 60\%$  SLGs  
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45 for  $c \sim 0.012$ g/L. The yield can be increased up to  $\sim 80\%$  if combined with density gradient ul-  
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47 tracentrifugation.<sup>60</sup> The flake size of LPE graphene in water-surfactant dispersions is on average  
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49 smaller ( $\sim 200$ nm,<sup>97</sup>  $\sim 30$ nm<sup>59</sup>) than thus far reported for NMP ( $\sim 1$  $\mu$ m<sup>55,58</sup>). The viscosity at room  
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51 temperature of NMP ( $1.7$ mPas<sup>86</sup>) is higher than water ( $\sim 1$ mPas<sup>86</sup>). Larger flakes dispersed in a  
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53 higher viscosity medium (such as NMP) experience higher frictional force<sup>98,99</sup> and sedimentation  
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55 coefficient<sup>99,100</sup> that make it more difficult for FLGs to sediment during ultracentrifugation. This  
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57 reduces the yield of SLGs in NMP compared to water.  
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Figure 3a plots a typical Raman spectrum of the ink dispensed on Si/SiO<sub>2</sub> and annealed at 170°C to remove NMP. Besides the G and 2D peaks, it shows significant D and D' intensities and the combination mode D+D' ~2950cm<sup>-1</sup>. The G peak corresponds to the E<sub>2g</sub> phonon at the Brillouin zone centre. The D peak is due to the breathing modes of sp<sup>2</sup> rings and requires a defect for its activation by double resonance (DR).<sup>93,101,102</sup> The 2D peak is the second order of the D peak. This is a single band in SLG,<sup>93</sup> whereas it splits in four in BLG, reflecting the evolution of the band structure.<sup>93</sup> The 2D peak is always seen, even when no D peak is present, since no defects are required for the activation of two phonons with the same momentum, one backscattering from the other.<sup>93</sup> DR can also happen intra-valley, *i.e.* connecting two points belonging to the same cone around **K** or **K'**.<sup>101-103</sup> This gives the D' peak. The 2D' is the second order of the D' peak.

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We assign the D and D' peaks to the edges of the sub-micrometer flakes,<sup>104</sup> rather than to the presence of a large amount of disorder within them. This is further supported by the plot of the G peak dispersion, Disp(G)(Figure 3b) (see Methods). In disordered carbons Pos(G) increases as the excitation wavelength decreases, from IR to UV,<sup>101</sup> thus Disp(G) increases with disorder.<sup>101,105</sup> The full width at half maximum of the G peak, FWHM(G), always increases with disorder.<sup>106,107</sup> Thus, combining I(D)/I(G), FWHM(G) and Disp(G) allows us to discriminate between disorder localized at the edges, and disorder in the bulk of the samples. In the latter case, to higher I(D)/I(G) would correspond higher FWHM(G) and Disp(G). Figure 4 a,b) show that Disp(G), I(D)/I(G) and FWHM(G) are not correlated, a clear indication that the major contribution to the D peak comes from the sample edges. Also, Disp(G) is nearly zero for all samples, compared to the values bigger than 0.1cm<sup>-1</sup>/nm expected for disordered carbons,<sup>105,108</sup> another indication of the lack of large structural disorder within our flakes. The distribution of Pos(2D), shown in Figure 3d, has two maxima ~2692 and 2705cm<sup>-1</sup>, similar to FWHM(2D) (Figure 3e). This is consistent with the samples being a distribution of SLG, BLG and FLGs, but with a significant fraction of SLGs. We note that for the flakes with the smallest Pos(2D) and FWHM(2D), the ratio of the 2D and G integrated areas, A(2D)/A(G), is at most 3.5, implying a doping of at least 10<sup>13</sup>cm<sup>-2</sup>.<sup>109-111</sup>

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We now estimate the  $\eta$ ,  $\rho$  and  $\gamma$  for our graphene-ink, in order to check its viability.  $\eta$  can be

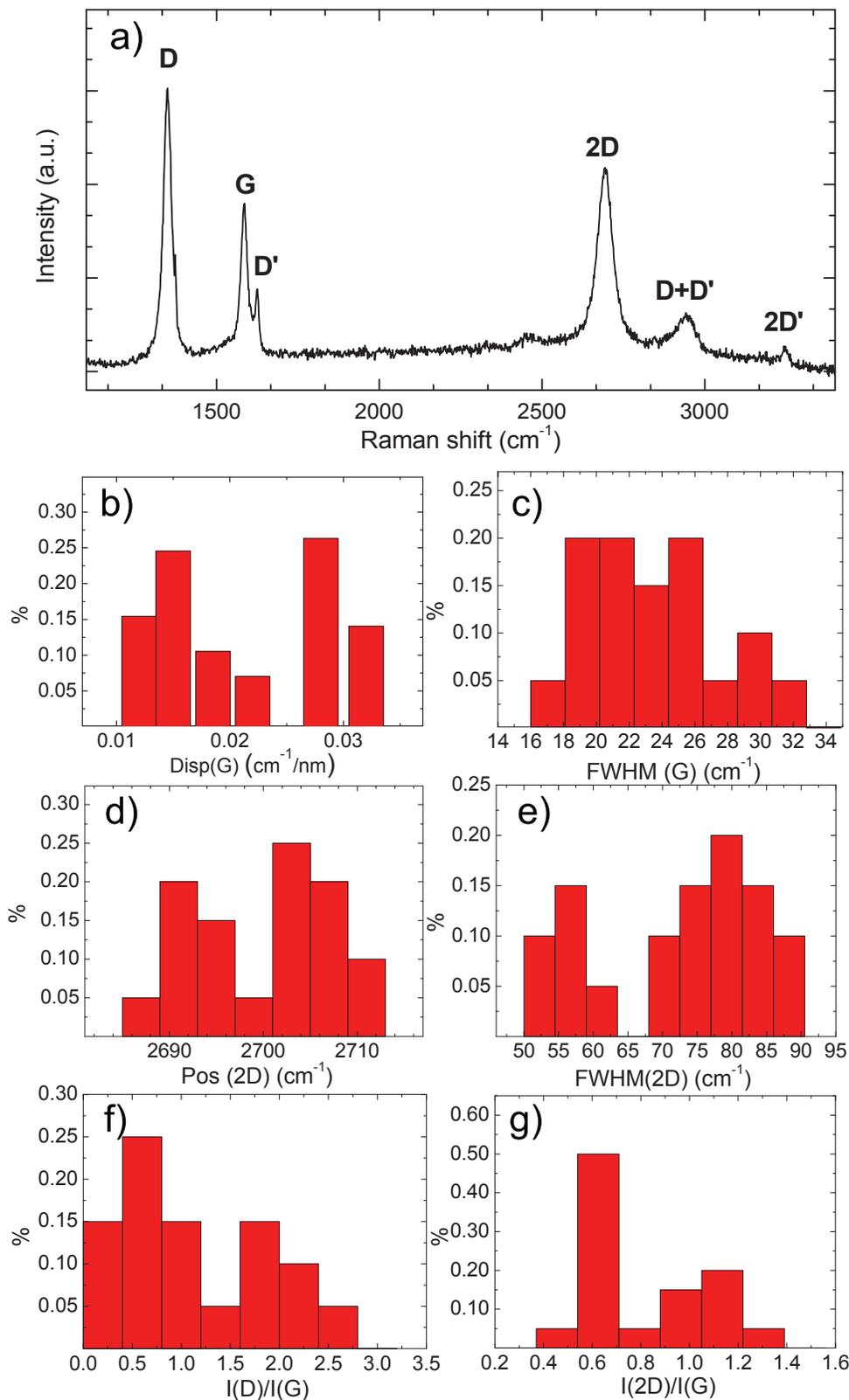


Figure 3: a) Raman spectrum of graphene-ink deposited on Si/SiO<sub>2</sub> at 514.5nm excitation. Distribution of b) Disp(G), c) I(D)/I(G), d) FWHM(G), e) Pos(2D), f) FWHM(2D), g) A(2D)/A(G).

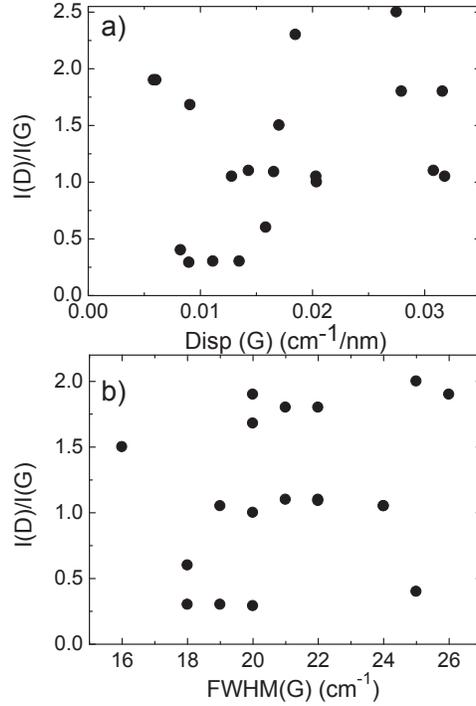


Figure 4: a)  $I(D)/I(G)$  as function of Disp(G), b)  $I(D)/I(G)$  as function of FWHM(G) measured on flakes of our ink deposited on Si/SiO<sub>2</sub>.

evaluated as  $\eta = \eta_0(1+2.5\phi)$ ,<sup>82,112</sup> where  $\eta_0$  is the viscosity of the pure solvent and  $\phi$  the volume fraction of particles in the dispersion. We assume  $\eta_0 = \eta_{NMP} \sim 0.8\text{mPas}$ , the viscosity of pure NMP at  $\sim 80^\circ\text{C}$ <sup>86,113</sup> (the Temperature of the drops ejected from our printer<sup>114</sup>). We take  $\phi = 1 - \frac{Vol_{NMP}}{Vol_{ink}}$ , where  $Vol_{NMP}$  [ $\sim 0.972\text{ mm}^3$ ] is the volume of 1mg pure NMP and  $Vol_{ink}$  [ $\sim 1.07\text{ mm}^3$ ] is the volume of 1mg of our ink, both measured by a micropipette ( $\pm 2\text{nL}$  precision), at room temperature and pressure. We thus get  $\phi \sim 0.1$ , and  $\eta \sim 0.96\text{mPas}$ . We determine  $\rho \sim 1.13\text{gcm}^{-3}$  from the average weight over 20 measurements of  $100\mu\text{l}$  of ink, and derive  $\gamma \sim 50\text{mJ m}^{-2}$  from tensiometer measurements. Given these parameters, and our nozzle diameter  $\sim 50\mu\text{m}$ , we get  $Z \sim \frac{\sqrt{\gamma\rho a}}{\eta} \sim 2$ , which falls within the range suitable for printing,<sup>75,76</sup> but close to the lower boundary of allowed  $Z$ .<sup>75-77</sup> On one hand, our ink has higher viscosity compared to that of usual printable inks,<sup>82,112</sup> implying a lower probability of secondary drops ejection.<sup>75,82,112</sup> On the other hand, high viscosity may generate nanoparticle re-aggregation.<sup>112</sup>

## Ink-jet printed features

The final layout of printed nano-particle inks depends on the substrate SE,<sup>21,23</sup> as well as ink viscosity and surface tension.<sup>21</sup>

To investigate the influence of surface treatments, we print our ink on pristine, HMDS coated and O<sub>2</sub> plasma treated Si/SiO<sub>2</sub>. A modified Epson Stylus 1500 ink-jet printer with a S020049 cartridge is used to print the dispersions under a constant nitrogen flow, followed by annealing at 170°C for 5 minutes to remove the NMP. The nozzle is placed ~1mm above the substrate. HMDS is deposited by spin coating for 40s at 1000rpm, followed by annealing at 80°C for 2 min. Alternatively the substrates are cleaned by a RF O<sub>2</sub> plasma at 200W and  $4 \times 10^{-1}$  Torr for 2 min.

We use optical micrographs to visualize the ink-jet printed drops, Figure 5a,b,c. The bright green/blue color of the printed features is due to the use of dark field imaging. These reveal that HMDS constrains the drops to 90μm diameter (Figure 5c), smaller than on the other substrates (~100μm and ~150μm for pristine, Figure 5b, and plasma treated SiO<sub>2</sub>, Figure 5a). As discussed above, we use NMP as solvent to reduce the coffee ring effect compared to low boiling point solvents (e.g. water, chloroform).<sup>18,82,84</sup> However, we still observe coffee-rings when printing on pristine SiO<sub>2</sub> (Figure 5b), while Figure 5c reveals a higher flake uniformity, and no coffee-rings on HMDS treated SiO<sub>2</sub>. Thus, HMDS appears to prevent coffee-rings. To understand this, we measure the substrates SE and investigate the printed stripes morphology, before and after surface treatment.

We utilize contact angle analysis to estimate the substrate surface tension and SE.  $\theta_C$  depends on the liquid surface tension<sup>79-81</sup> and the substrate critical surface tension,<sup>79-81</sup> according to the Young's relation<sup>79,81,115</sup>  $\gamma_{SV} - \gamma_{SL} - \gamma_{LV} \cos \theta_C = 0$ , where  $\gamma_{SV}$  [mJ m<sup>-2</sup>] is the solid-vapor surface tension,  $\gamma_{SL}$  is the solid-liquid surface tension and  $\gamma_{LV}$  is the liquid-vapor surface tension. Figure 5d is a Scanning Electron Microscope (SEM) micrograph of a representative printed pattern showing the viability of ink-jet printing to fabricate complex layouts.

Figure 6a,b show ink drops printed onto pristine and HMDS treated Si/SiO<sub>2</sub>, with  $\theta_C \sim 6^\circ$  and  $\sim 65^\circ$ , indicating that the pristine substrate SE is modified following HMDS treatment.  $\gamma_{LV}$

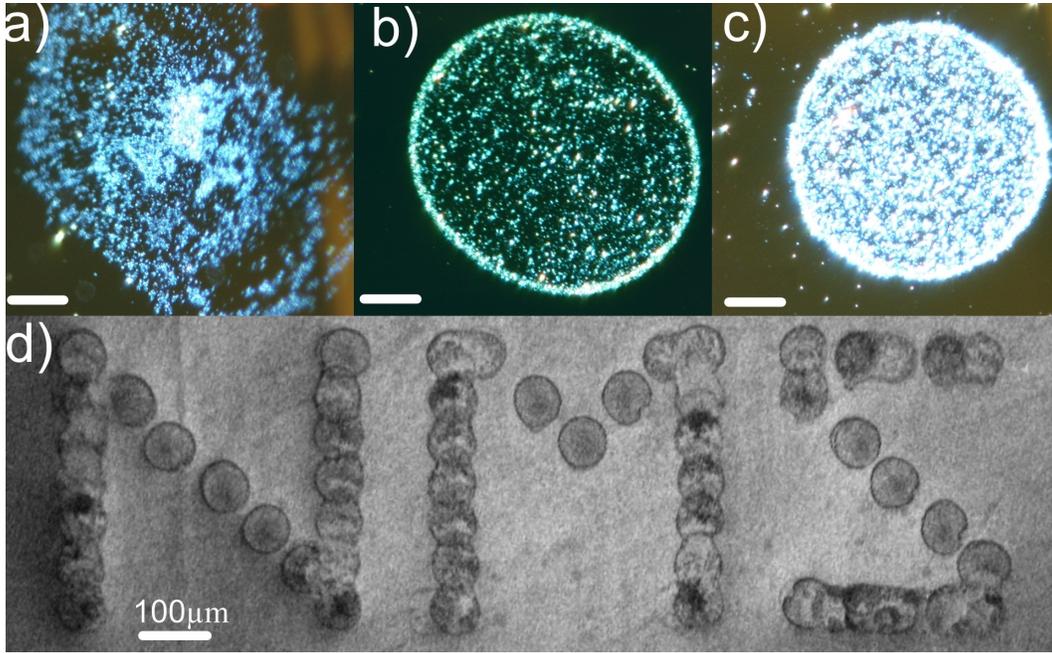


Figure 5: Dark field optical micrograph of inkjet printed drops on a) plasma cleaned, b) pristine and c) HMDS treated substrate. Scale is  $20\mu\text{m}$ . d) SEM micrograph of drops printed in a pattern.

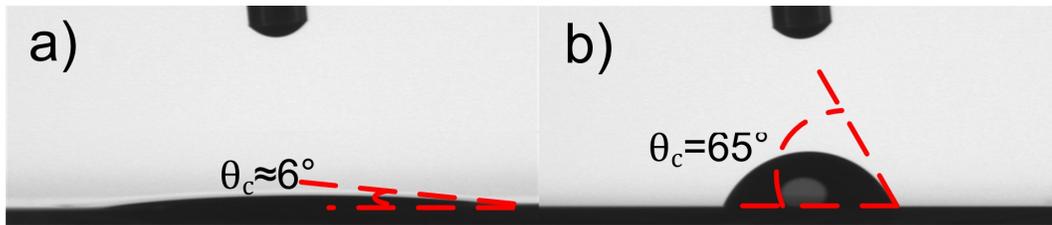


Figure 6: Images of water drops dispensed on a) pristine and b) HMDS treated  $\text{Si/SiO}_2$  substrates

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3 was measured  $\sim 73 \text{ mJ m}^{-2}$  in Ref.<sup>116</sup> for DI water, whereas  $\gamma_{SV} \sim 143.50 \text{ mJ m}^{-2}$  and  $\sim 20 \text{ mJ m}^{-2}$   
4 were reported for pristine<sup>116</sup> and HMDS treated<sup>116</sup> Si/SiO<sub>2</sub> substrates. Consequently,  $\gamma_{SL} \sim 73 \text{ mJ}$   
5  $\text{m}^{-2}$  and  $\sim 29 \text{ mJ m}^{-2}$  for pristine and HMDS treated Si/SiO<sub>2</sub>, respectively. A higher  $\gamma_{SL}$  implies a  
6 higher SE.<sup>80,117</sup> Indeed, our  $\gamma_{SL}$  correspond to SEs  $\sim 120$  and  $\sim 50 \text{ mJ m}^{-2}$  for pristine and HMDS  
7 treated Si/SiO<sub>2</sub>. A small  $\theta_C$  results in the drop rapid spreading on the substrate,<sup>79</sup> as seen in pristine  
8 SiO<sub>2</sub>. On the other hand, HMDS provides higher  $\theta_C$ , since it lowers  $\gamma_{SL}$  (thus the substrate SE),  
9 therefore reducing the wettability.<sup>80,117</sup>

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When ink-jet printing stripes, the inter-drop (i.e. centre to centre) distance is an important parameter.<sup>118</sup> For a large distance, individual drops are deposited on the substrate.<sup>75,82,118</sup> As the inter-drop distance decreases, these merge into a line.<sup>118</sup> Thus, in order to obtain a continuous line we need an inter-drop distance smaller than the drop diameter.<sup>118</sup> On the other hand, Refs.<sup>82,112</sup> reported that a very small inter-drop distance can result in particle aggregation on the substrate, giving a non-uniform stripe (i.e. irregular edges). We thus select an inter-drop distance suitable to have continuous lines, avoiding at the same time non-uniformities and irregular edges.

Figure 7a,b,c are optical images of printed stripes on pristine, O<sub>2</sub> plasma treated and HMDS treated Si/SiO<sub>2</sub>, whereas Figure 7d,e,f plot the respective Atomic Force Microscope (AFM) topographies. The stripe in Figure 7a is  $\sim 100\text{-}110 \mu\text{m}$  wide, has an average thickness  $\sim 70 \text{ nm}$  and an irregular flake distribution, with aggregation of flakes. That in Figure 7b is wider ( $\sim 130\text{-}140 \mu\text{m}$ ), with aggregates at the edges, and an average thickness  $\sim 55 \text{ nm}$ . The stripe in Figure 7c has a more uniform and regular distribution of flakes, having  $\sim 85\text{-}90 \mu\text{m}$  width and  $\sim 90 \text{ nm}$  average thickness. The width narrows going from the O<sub>2</sub> plasma treated to the HMDS treated Si/SiO<sub>2</sub>, due to the SE decrease. Figure 7d,e show stripes with voids and irregular flake distribution, with  $R_z \sim 30\text{-}40 \text{ nm}$ . Figure 7f presents a more homogeneous network with  $R_z \sim 15 \text{ nm}$ . Thus,  $R_z$  is lower when  $\theta_C$  is higher, because the poor wettability of drops with higher  $\theta_C$  reduces the stripe diameter (as shown in Figure 7a,b,c), confining the flakes onto a smaller area. The uniformity of stripes printed on the HMDS treated substrate corroborates the above considerations on the SE changes. In fact, the presence of silane groups in the molecular structure of HMDS<sup>85</sup> acts as promoter of metallic par-

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ticles adhesion to the substrate.<sup>85,119</sup> Analogously, HMDS may promote the adhesion of graphene flakes to the substrate, thus favoring the formation of a regular network.

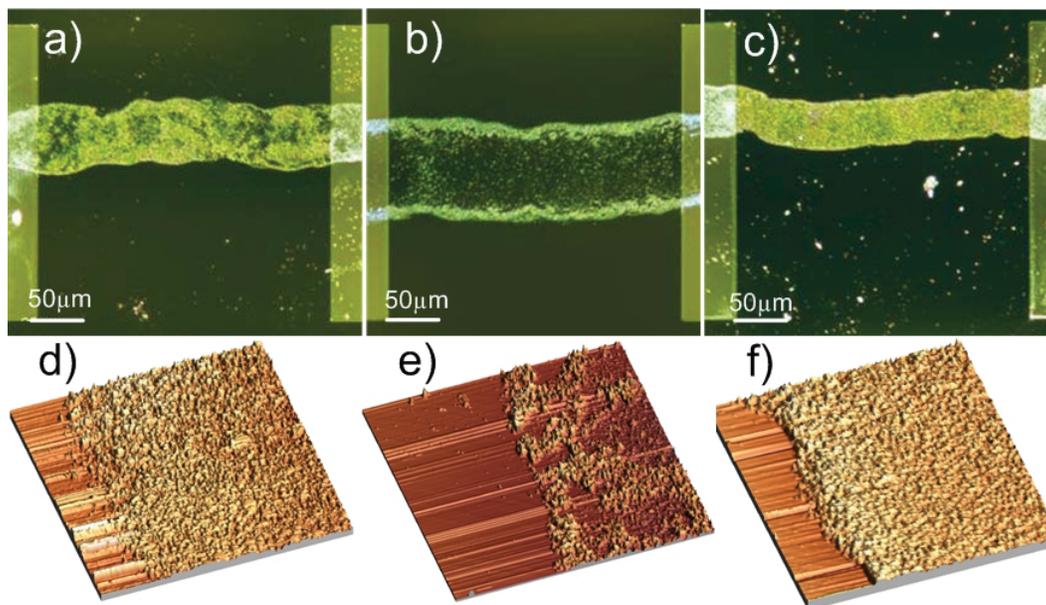
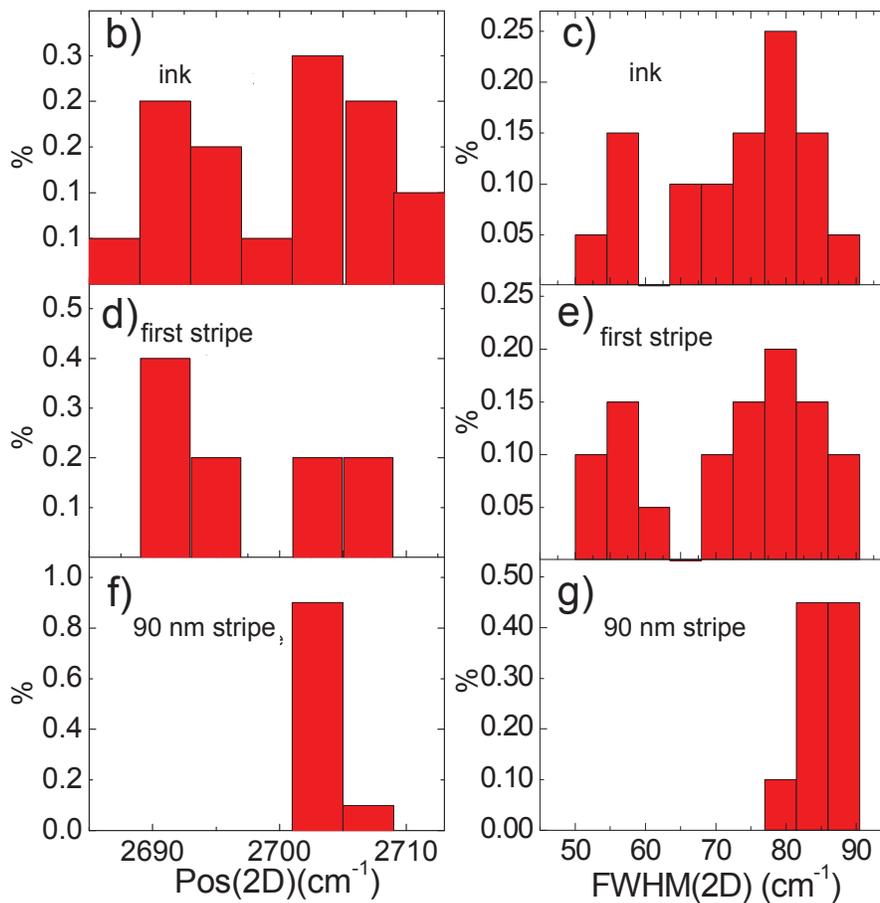
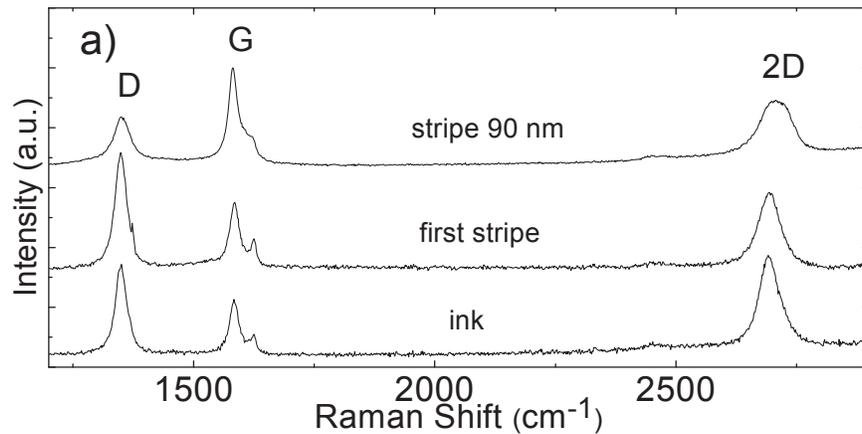


Figure 7: Optical micrograph of ink-jet printed stripes on a) pristine, b) O<sub>2</sub> and c) HMDS treated substrates. d, e, f) AFM images of a, b, c, respectively.

Figure 8a compares a typical Raman spectrum of a flake in the ink, with a measurement on the first stripe and on a stripe 90 nm thick, after 30 printing repetitions. Spectra are acquired after annealing at 170°C to remove the NMP. Figure 8b, c, d, e, f, g and Figure 9 compare the Pos(2D), FWHM(2D) and Disp(G) distributions. The data show that the first stripe has very similar characteristics to the ink, as expected. However, the spectra after 90 repetitions show a Pos(2D) and FWHM(2D) distributions more typical of a multi-layer sample, having lost any direct signature of SLG. Note however that the 2D peak shape, even for the 90nm stripe, remains distinctly different from that of graphite. A similar aggregation of flakes was previously observed for thick films derived from graphene solutions.<sup>55</sup> In all cases Disp(G) remains similar, and very low, again showing the lack of large amounts of defects within the flakes.



52 Figure 8: a) Typical Raman spectrum of individual flakes in the ink, compared with spectra  
53 measured on the first stripe and on a stripe 90nm thick. Pos(2D) and FWHM(2D) distributions for  
54 b,c) ink; d,e) fist stripe; f,g) 90nm thick stripe.

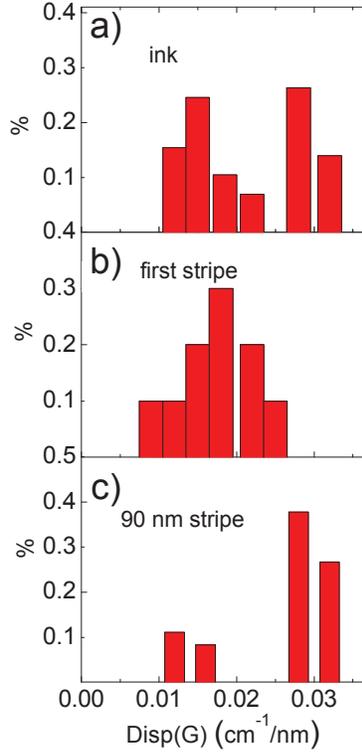


Figure 9: Distribution of Disp(G) for a) ink, b) first stripe, c) 90nm thick stripe

## Transparent and conductive patterns

We now investigate the viability of our ink to print transparent and conductive patterns. We characterize the sheet resistance  $R_s$  [ $\Omega/\square$ ] and Transmittance  $T$  [%] of our stripes when placed on a transparent substrate. We thus use pristine,  $O_2$  and HMDS treated borosilicate glass, with  $R_z < 15\text{nm}$  similar to  $\text{SiO}_2$  on Si, but with  $T \sim 99\%$  (Pyrex 7740-Polished Prime Grade).

Figure 10a shows that for our stripes the thickness ( $t$ ) increases linearly as a function of printing repetitions, with a slope defined by the surface treatment. Figure 10b plots the four-probe measured  $R_s$  (see Methods) as a function of  $t$ . For large  $t$ ,  $R_s$  settles to  $\sim 34\text{k}\Omega/\square$ ,  $\sim 500\text{k}\Omega/\square$ , and  $\sim 10^5\text{k}\Omega/\square$  for HMDS treated, pristine and  $O_2$  treated glass, respectively. For  $t < 20\text{nm}$ ,  $R_s$  increase for all substrates. For a thin film,  $R_s = (\sigma t)^{-1}$ , where  $\sigma$  [S/m] is the conductivity.<sup>120</sup> Thus, from Figure 10b and  $\sigma = (R_s t)^{-1}$ , we get the data in Figure 10c.  $\sigma$  is constant for  $t > 20\text{nm}$ , in the case of HMDS treated, pristine and plasma treated glass, with an average  $\sigma \sim 10^2\text{S/m}$ ,  $\sim 30\text{S/m}$ , and  $\sim 10^{-1}\text{S/m}$ , respectively. Thus, stripes on HMDS treated glass have an higher  $\sigma$  combined

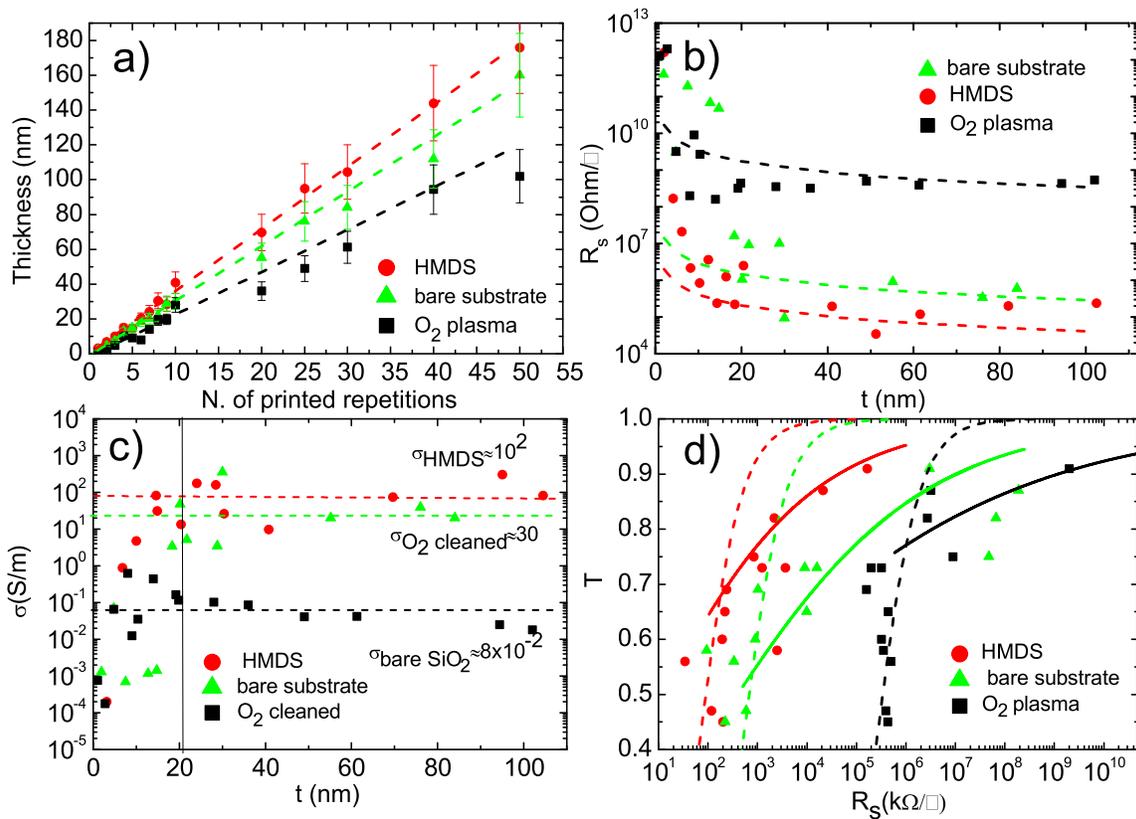


Figure 10: a) Thickness as a function of printing repetitions. b,c)  $R_s$ ,  $\sigma$  as a function of thickness. d)  $T$  as a function of  $R_s$  for HMDS coated (red dots), O<sub>2</sub> plasma treated (green triangles) and pristine (black squares) substrates

with a more regular network of flakes, compared to the other two substrates. When  $t < 20\text{nm}$ ,  $\sigma$  decreases for all substrates. A similar trend was reported for CNT films on  $\text{SiO}_2$  (produced by vacuum filtration),<sup>121,122</sup> ink-jet printed CNT patterns on  $\text{SiO}_2$ ,<sup>29,30</sup> graphene films on  $\text{SiO}_2$ ,<sup>123,124</sup> and Polyethylene-terephthalate(PET),<sup>123,124</sup> as well as Ag nanowire films, produced by vacuum filtration on  $\text{SiO}_2$ .<sup>123</sup> Refs.<sup>121–124</sup> explained this decrease of  $\sigma$  for small  $t$ , due to percolation.

The percolation theory<sup>125</sup> predicts  $\sigma$ , for a network of conductive particles, to scale as:<sup>125</sup>

$$\sigma \propto (X - X_c)^\beta \quad (1)$$

where  $X$  [ $\mu\text{g}/\text{mm}^2$ ] is the concentration of conductive particles per unit area,  $X_c$  [ $\mu\text{g}/\text{mm}^2$ ] is the critical concentration of flakes corresponding to the percolation threshold and  $\beta$  is the percolation exponent. Eq. (1) can be rewritten in terms of  $t$ , rather than  $X$ <sup>121</sup> as:

$$\sigma \propto (t - t_c)^\varepsilon \quad (2)$$

where  $t_c$  is the critical thickness and  $\varepsilon$  is the percolation exponent. Figure 10c shows two regimes for  $\sigma$  as a function of  $t$ : a percolative linear behavior for  $t < 20\text{nm}$  and a constant  $\sigma_{bulk}$  for  $t > 20\text{nm}$ . Such regimes can be explained considering that our films stop behaving like bulk materials below a critical thickness ( $t_{min}$ ), entering the percolation region.

The exponent  $\varepsilon$  can be estimated by a linear fit of the  $\log_{10}$  plot of  $\sigma$  vs  $t$ , in the percolation region ( $t < 20\text{nm}$ ), Figure 11. We get  $\varepsilon \sim 4$  for stripes on HMDS treated and pristine glass, while  $\varepsilon \sim 3$  for  $\text{O}_2$  treated glass. These values indicate percolation, as reported by Refs.<sup>123,126–128</sup> for networks with various geometries.  $\varepsilon$  is expected to increase with particle size<sup>127,128</sup> and decrease with  $X_c$ .<sup>127,128</sup> Assuming a similar particle size, since the same ink is used for all cases, we deduce that  $\varepsilon \sim 4$  points to a smaller  $X_c$  than  $\varepsilon \sim 3$ . This indicates formation of a more uniform network on HMDS treated and pristine glass compared to  $\text{O}_2$  treated glass.

We also determine the minimum concentration necessary to achieve the bulk conductivity regime. To do this we assume  $X \gg X_c$ , because the bulk regime needs a tight network of intercon-

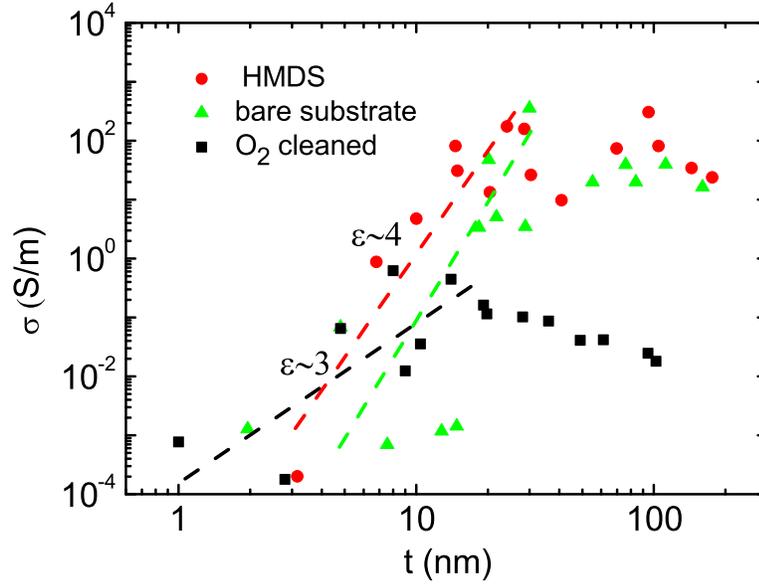


Figure 11: Conductivity as a function of film thickness, in logarithmic scale, for stripes printed on HMDS treated (red dots), O<sub>2</sub> treated (green triangles) and pristine (black squares) substrates. Lines are fits in the percolation regime of conductivity.

nected flakes.<sup>123,126,129</sup> Given our  $c \sim 0.11$  g/L, volume per printed drop  $\sim 10$  nL,<sup>114</sup> and a dried drop size on the three substrates of  $\sim 90, 100, 130$   $\mu\text{m}$ , we estimate  $X \sim 4 \times 10^{-2}, \sim 10^{-2}$  and  $\sim 0.7 \times 10^{-2}$   $\mu\text{g}/\text{mm}^2$  for stripes printed on HMDS, pristine and plasma treated glass, respectively. Consequently, from Eq. (1),  $\sigma$  for stripes printed on HMDS treated glass ( $\sigma \sim 10^2$  S/m) is higher than on pristine ( $\sigma \sim 40$  S/m) and plasma treated glass ( $\sigma \sim 0.1$  S/m).

Figure 10d plots  $T$  as a function of  $R_s$ . The dashed lines are a plot of the relation  $T = \left(1 + \frac{Z_0 G_0}{2R_s \sigma_{bulk}}\right)^{-2}$  expected for graphene-ink stripes with  $\sigma_{bulk}$  conductivity, where  $Z_0 = 377 \Omega$  is the free-space impedance,  $G_0 \sim 6 \times 10^{-5} \Omega^{-1}$  is the universal optical conductance of graphene.<sup>130</sup> The solid lines are a plot of  $T = \left[1 + \frac{1}{\Pi} \left(\frac{Z_0}{R_s}\right)^{1/(\epsilon+1)}\right]^{-2}$  expected for stripes in the percolative regime,<sup>123</sup> where  $\Pi$  is the percolative Figure of Merit  $\Pi = 2 \left[\frac{\sigma_{bulk}/G_0}{(Z_0 t_{min} G_0)^\epsilon}\right]^{1/(\epsilon+1)}$ . Our experimental  $T$  deviates from the dashed lines for  $T > 75\%$ . We assign this to the percolative regime, with  $\sigma_{DC}$  deviating from a bulk-like behavior. Also in this case, printing on HMDS treated glass gives the highest  $T$  for a given  $R_s$ .

## Ink jet printed devices

Ink-jet printed TFTs based on organic semiconducting polymers have been widely investigated.<sup>15,131,132</sup> The current state of the art devices have  $\mu$  ranging from 0.01 to  $\sim 0.5\text{cm}^2\text{V}^{-1}\text{s}^{-1}$ , with ON/OFF ratios up to  $10^5$ .<sup>131-133</sup> Several inkjet printed TFTs using various carbon nanomaterials have been reported. For example, fullerene-based TFTs were discussed in Refs.,<sup>134,135</sup> with  $\mu$  up to  $0.01\text{cm}^2\text{V}^{-1}\text{s}^{-1}$  and an ON/OFF ratio  $< 10$ . TFTs printed from SWNT-based inks have been presented by several groups.<sup>27-29,31,32</sup> The highest  $\mu$  reported thus far is  $\sim 50\text{cm}^2\text{V}^{-1}\text{s}^{-1}$  combined with an ON/OFF ratio  $10^3$ , but measured at  $10^{-6}$  Torr and 100K.<sup>32</sup> Ink-jet printed TFTs from GO-based inks were discussed in Refs.,<sup>72,73</sup> with  $\mu$  up to  $\sim 90\text{cm}^2\text{V}^{-1}\text{s}^{-1}$  for an ON/OFF ratio of 10 (measured at room conditions), after GO reduction.

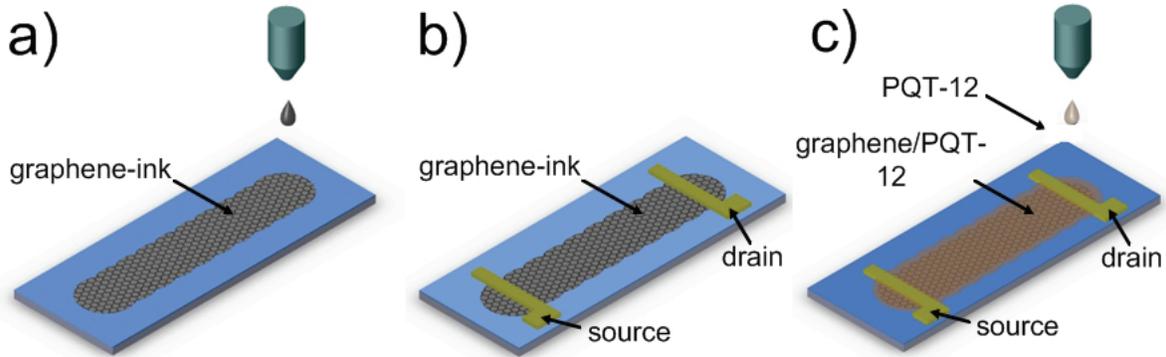


Figure 12: a) Graphene-ink on Si/SiO<sub>2</sub>. b) Two Cr-Au pads define the source and drain contacts. c) A layer of Poly[5,5'-bis(3-dodecyl-2-thienyl)-2,2'-bithiophene] (PQT-12) is printed on top.

We print our TFTs as for Figure 12a, and contact them with chromium-gold source and drain pads (Figure 12b). The transfer characteristics are measured (at room conditions) at different drain voltages ( $V_d = -2, -4, -8\text{V}$ ). We get  $\mu$  from the slope of the transfer-characteristic according to  $\mu = \frac{L}{W C_i V_d} \frac{dI_d}{dV_g}$ , where  $L$  [ $\mu\text{m}$ ] and  $W$  [ $\mu\text{m}$ ] are the channel length and width respectively,  $C_i$  is the gate dielectric capacitance ( $\sim 10\text{nF/cm}^2$ ).<sup>136</sup> This corresponds to  $\mu \sim 95\text{cm}^2\text{V}^{-1}\text{s}^{-1}$  and ON/OFF ratio  $\sim 10$  at  $V_d = -8\text{V}$ , comparable to those reported in Ref.<sup>73</sup> for ink-jet printed RGO TFTs.  $\mu$  in our devices is almost four times higher than printed fullerene-based TFTs<sup>134,135</sup> (for the same ON/OFF ratio) and more than two orders of magnitude higher than that reported for ink-jet printed

SWNTs<sup>27,29</sup> (for a on/off ratio of 10). However, the ON/OFF ratio in our TFTs is lower than the state of the art for SWNTs (but measured at  $10^{-6}$  Torr and 100K) at similar  $\mu$ .<sup>32</sup> We note that ink-jet printed electronics requires high  $\mu$  at room conditions.<sup>11,18</sup> So far SWNT ink-jet printed devices measured at room conditions have  $\mu$  no larger than  $\sim 1\text{cm}^2\text{V}^{-1}\text{s}^{-1}$  (at ON/OFF ratio $\sim 10$ ),<sup>29</sup> which is two orders of magnitude smaller than our graphene ink-jet printed TFTs.

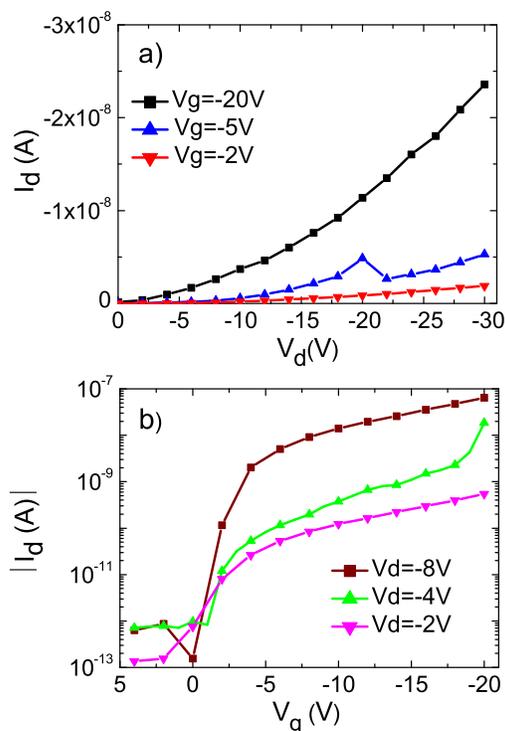


Figure 13: a) Output characteristics and b) transfer characteristic of an ink-jet printed graphene/PQT TFT.

Organic semiconducting inks<sup>131–133</sup> suffer from low  $\mu$ , limited by variable range hopping of charges between the isolated polymer chains.<sup>137</sup> The overall charge conduction in crystalline organic semiconducting thin films is determined by both intra-chain and inter-chain charge transport.<sup>138</sup> The intrachain transport is much faster than inter-chain hopping.<sup>137,138</sup> Many groups have tried to improve interchain hopping.<sup>27,28,139,140</sup> Ref.<sup>139</sup> proposed a chemical modification of the semiconducting organic ink by electron acceptor, while embedding Au nano-particles in the semiconducting organic ink was proposed in Ref.<sup>140</sup> Embedding SWNTs in the semiconducting ink allowed us to get  $\mu \sim 0.07\text{cm}^2\text{V}^{-1}\text{s}^{-1}$  at room conditions.<sup>27,28</sup>

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4 We combine our graphene-ink with one of the most common organic polymer in ink-jet print-  
5 ing, Poly[5,5'-bis(3-dodecyl-2-thienyl)-2,2'-bithiophene] (PQT-12)<sup>131-133</sup> in order to investigate  
6 its viability as interchain hopping enhancer. PQT-12 is widely used due to the higher environmen-  
7 tal stability (up to 300 days at room conditions<sup>141</sup>), with respect to other organic semiconducting  
8 inks.<sup>140,141</sup> Graphene can bridge the polymer chains, allowing more efficient charge transport.

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10 We fabricate a graphene/PQT-12 TFT following the steps shown in Figure 12a,b,c. Figure 13a  
11 plots its output characteristics at  $V_g = -2, -5, -20$  V. For each  $V_g$ ,  $V_d$  is swept from 0 to -30 V in steps  
12 of 2V. At  $V_d = -8$  V, we get  $\mu \sim 0.2 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$  and an ON/OFF ratio  $\sim 4 \times 10^5$ . This  $\mu$  is about ten  
13 times that for ink-jet printed SWNTs/PQT-12 TFTs<sup>27,28</sup> at an ON/OFF ratio  $\sim 10^5$ . When compared  
14 to pure organic semiconducting polymers, our  $\mu$  is 20 times higher than ink-jet printed PQT-  
15 12,<sup>132,133</sup> and twice the highest reported  $\mu$  for ink-jet printed TFT made of pure (Poly(2,5-bis(3-  
16 tetradecylthiophen-2-yl)thieno[3,2-b]thiophene)).<sup>18,140,142,143</sup> Thus, the combination of graphene-  
17 and organic semiconducting- inks is promising for high performance printed electronics.

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We demonstrated ink-jet printing of graphene. Liquid phase exfoliated graphene is an ideal and low cost material for the fabrication of transparent conductive inks. Our graphene-ink was used to print TFTs with  $\mu$  up to  $\sim 95 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$ . It was also combined with PQT-12 to fabricate devices with  $\mu \sim 0.2 \text{ cm}^2 \text{ V}^{-1} \text{ s}^{-1}$  and ON/OFF ratios  $\sim 4 \times 10^5$ . This demonstrates the viability of graphene-inks for flexible and transparent electronics.

## Methods

### Raman spectroscopy

The centrifuged dispersions are diluted and drop-cast onto a Si wafer with 300nm thermally grown SiO<sub>2</sub> (LDB Technologies Ltd.). These samples are then used for Raman measurements,

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3 collected with a Renishaw 1000 at 457, 514.5 and 633nm and a 100× objective, with an incident  
4 power of ~1mW. The G peak dispersion is defined as  $\text{Disp}(G) = \Delta \text{Pos}(G) / \Delta \lambda_L$ , where  $\lambda_L$  is the  
5 laser excitation wavelength. Disp(G) is generated from the linear fit the plot of Pos(G) as a function  
6 of the laser excitation wavelength.  
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### 11 12 13 **Contact angle and surface tension measurements** 14

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16 A KSV CAM200 stage is used for contact angle and surface tension measurements. The con-  
17 tact angle is measured by dispensing 1μl ultrapure DI water on the substrates and measuring the  
18 angle at which the ink interface meets the solid surface. The surface tension is measured by the  
19 DuNouy-Padday technique.<sup>144</sup> This consists in using a rod few millimeters diameter immersed in  
20 the dispersion, followed by pull out. The rod is attached to a scale or balance via a thin metal hook  
21 that measures the maximum pull force. This is recorded as the probe is first immersed 1mm into  
22 the solution and then slowly withdrawn from the interface.  
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### 31 32 **Optical transmittance** 33

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35 The transmittance is measured on samples ink-jet printed on borosilicate glass (Pyrex 7740 -  
36 Polished Prime Grade) followed by annealing at 170°C for 1h by scanning a 514.5nm laser beam  
37 onto the sample at 100μm steps. The transmitted beam is measured with a photodiode. An optical  
38 microscope equipped with 100× long-distance objective focuses the laser on the sample down to  
39 a spot size of ~2μm (incident power on the sample ~8mW). The transmitted power intensity is  
40 measured by a Ophir Nova II power meter with 0.1μW resolution.  
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### 48 49 **Electrical measurements** 50

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52 Electrical measurements to characterize the printed devices are performed using a cascade at-  
53 toguard probe station equipped with an Agilent Semiconductor Parameter Analyzer 4156C. The  
54 integration time is set to 500μs and the delay time is set to 50ms to ensure that no transient insta-  
55 bilities in the current occur.  
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